



Amendments to the Specification

IN THE ABSTRACT OF THE DISCLOSURE

Attached hereto is a replacement Abstract with markings to show amendments.

IN THE WRITTEN DESCRIPTION

Please replace the BACKGROUND OF THE INVENTION, SUMMARY OF THE INVENTION, BRIEF DESCRIPTION OF THE DRAWINGS AND DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT sections with the marked-up copy of the sections enclosed herewith. This includes page 1, line 1, through page 19, line 20, of the present specification.

Please replace the paragraph beginning at page 27, line 1, with the following rewritten paragraph:

As shown in Table 4, Specimen No. 11 developed recrystallization during the extrusion and exhibited reduced strength due to a low Mn content. ~~The~~ Specimen No. 11 also produced stress corrosion cracking at 120 hours into the test. Specimen No. 12 developed coarse intermetallic compounds due to the existence of excessive Mn, which resulted in a decreased elongation. Specimen No. 13 exhibited poor corrosion resistance since the composition does not fall into the range specified for the total content of Si% + Mg% + Cu%. Specimens No. 14 and No. 15 showed poor corrosion resistance since the compositions failed to satisfy the range specified for Mg and $Mg\% \leq 1.7 \times Si\%$, respectively. Specimens No. 16 and No. 17 exhibited poor corrosion resistance and elongation since the compositions failed to satisfy the range specified in the present invention for the total content of Mg and Si and the Si content, respectively. Specimen No. 18 showed poor corrosion resistance due to a high Cu content.

Please replace the paragraph beginning at page 32, line 19, with the following rewritten paragraph:

The Specimen No. 33 could not be prepared since the extrusion had to be aborted due to ~~a~~-die bearing breakage caused by the short bearing length of the solid die. In the Specimen No. 34, recrystallization occurred in the surface layer due to an increased extrusion temperature since the bearing length of the solid die was long, whereby satisfactory strength could not be obtained. Moreover, since the resulting extruded product developed cracks, the intergranular corrosion test and the stress corrosion cracking test could not be performed.

Please replace the paragraphs beginning at page 36, line 1, with the following rewritten paragraphs:

As shown in Table 7, Specimens No. 36 to No. 45 according to the present invention demonstrated a high strength, excellent corrosion resistance, and excellent stress corrosion cracking resistance.

Comparative Example 3

Aluminum alloys having compositions shown in Table 8 were cast by semi-continuous casting to prepare billets with a diameter of 200 mm. The billets were treated according to the same procedures as in Example 3 to prepare extrusion billets. The extrusion billets were heated to 520°C and extruded under the identical conditions as in Example 1 and using the same porthole die as in Example 3, to obtain tubular extruded products having a tubular profile. The tubular extruded products were treated according to the same procedure as in Example 3 to refine the products to T6 temper. Properties of the T6 materials were evaluated in the same manner as in Example 3 by (1) the measurement of the area fraction of the fibrous structure in the transverse cross section, (2) the tensile test, (3) the intergranular corrosion test, and (4) the stress corrosion cracking test. The evaluation results

are summarized in Table 9. In Tables 8 and 9, values and test results that fall outside of the ranges specified in the present invention are underscored.

Please replace the paragraph beginning at page 39, line 1, with the following rewritten paragraph:

As shown in Table 9, Specimen No. 46 developed recrystallization during the extrusion and exhibited reduced strength due to low Mn content. The Specimen No. 46 also produced stress corrosion cracking at 120 hours into the test. Specimen No. 47 developed coarse intermetallic compounds due to the existence of excessive Mn, which resulted in decreased elongation. Specimen No. 48 exhibited poor corrosion resistance since the composition did not fall into the range specified for the total content of Si% + Mg% + Cu%. Specimens No. 49 and No. 50 showed a poor corrosion resistance since the compositions failed to satisfy the range specified for the Mg content and $Mg\% \leq 1.7 \times Si\%$, respectively. Specimens No. 51 and No. 52 exhibited poor corrosion resistance and poor elongation since the compositions failed to satisfy the range specified in the present invention for the total content of Mg and Si and the Si content, respectively. Specimen No. 53 showed poor corrosion resistance due to high Cu content.

Please replace the paragraph beginning at page 40, line 19, with the following rewritten paragraph:

Comparative Example 4

The aluminum alloy A having the composition shown in Table 1 was cast by semi-continuous casting to prepare billets with a diameter of 200 mm. The billets were treated under conditions shown in Table 10 to obtain tubular extruded products. In treatments No. i2 to No. o2, extrusion was performed using the same porthole die as that used in Example 3. In ~~a~~-treatment No. p2, a porthole die in which the ratio of the chamber depth D to the bridge width W was 0.43 (i.e. $W/D = 0.43$) was used.

Please replace the paragraphs beginning at page 44, line 1, with the following rewritten paragraphs:

As shown in Table 11, Specimens No. 54 to 64 according to the manufacturing conditions of the present invention demonstrated high strength, excellent corrosion resistance, and excellent stress corrosion cracking resistance. By contrast, Specimens No. 65 to 70 showed defects in either one of the evaluation tests for strength, corrosion resistance, and stress corrosion cracking resistance. Namely, the Specimen No. 65 exhibited insufficient post-quenching strength along with reduced corrosion resistance since the cooling rate after homogenization was not adequately high. ~~The~~ Specimen No. 66 showed an insufficient strength and decreased corrosion resistance since the low extrusion temperature failed to achieve sufficient dissolution of the solute elements.

~~The~~ Specimen No. 67 showed an inferior strength and decreased corrosion resistance since the cooling rate was low during the press quenching. ~~The~~ Specimen No. 68 revealed an inadequate strength and decreased corrosion resistance, resulting from its low cooling rate after the solution heat treatment. Since ~~the~~ Specimen No. 69 was extruded with a die having a high flow speed ratio, the billet was extruded at an excessively high temperature. This gave rise to a growth of a recrystallized grain structure, resulting in ~~the~~ an area-fraction of the fibrous structure to the cross-sectional structure ~~at~~ of 50%. As a result, the finished product failed to acquire a satisfactory strength and exhibited an intergranular corrosion and high weight loss, whereby cracking occurred at 500 hours into the stress corrosion cracking test.